

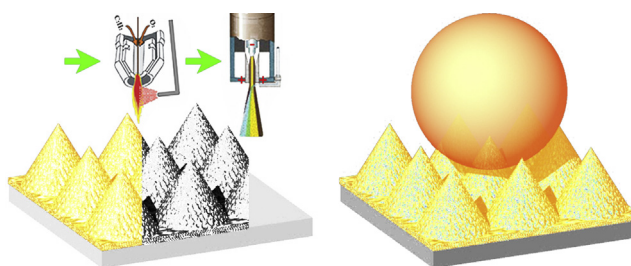
# Robust and easy-repairable superhydrophobic surfaces with multiple length-scale topography constructed by thermal spray route

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## HIGHLIGHTS

## GRAPHICAL ABSTRACT



## ARTICLE INFO

## ABSTRACT

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This paper demonstrates a thermal spray route for making superhydrophobic surfaces with mechanically robust and easy-repairable performances. Cone-like geometry with multi-scale topographical structures was firstly achieved by plasma spray deposition of titania using stainless steel mesh as shielding plate, then polytetrafluoroethylene/nano-copper composites were deposited by suspension flame spray onto the patterned titania coating. The coatings exhibit superhydrophobicity with a water contact angle of  $\sim 153^\circ$  and a sliding angle of  $\sim 2^\circ$ . Unlike the surfaces with normal structure, the coatings with multiple length-scale structure retain the superhydrophobicity even after severe mechanical abrasion. The superhydrophobicity can be further easily restored after it is damaged by abrasion. The thermal spray construction of superhydrophobic surfaces proposed in this research offers the advantages of precisely tailoring the surface textures and surface chemistry cost-efficiently over as large an area as desired, showing bright prospects for versatile applications.

## 1. Introduction

Superhydrophobic surfaces have drawn extensive interests from both academia and industry during the past decades due to their potential applications in various fields, for example anti-corrosion [1,2], anti-icing [3,4], self-cleaning [5,6], antifouling [7,8], and drag-reducing [9,10]. However, practical applications

of the superhydrophobic surfaces are usually restricted by their poor mechanical stability. In nature, plants retain their superhydrophobicity by reconstructing their surfaces with micro-/nano-hybrid structures and releasing wax-like materials after destroyed [11–13]. Yet it is almost impossible for the superhydrophobic surfaces made artificially to follow nature's way when destroyed. Therefore, fabrication of the superhydrophobic surfaces with favorable mechanical stability and easy reparability is to be developed towards accomplishing long-term functional applications.

To enhance their mechanical properties, the superhydrophobic surfaces with micro-/nano- hierarchical structures have been

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attempted. For example, Kondrashov et al. reported a mechanically robust superhydrophobic surface with hierarchical roughness consisting of silicon microcones and silicon nanograss, which was achieved by a cryogenic deep reactive ion etching process [14]. Emelyanenko et al. developed a durable superhydrophobic coating on stainless steel based on nanosecond IR laser micro- and nano-texturing with subsequent chemisorption of fluorooxysilane [15]. Groten et al. fabricated superhydrophobic surfaces with combined micro-/nano-scale structures by silicon etching and subsequent coating with a monolayer of fluoropolymer [16]. The abovementioned techniques offer the superhydrophobic surfaces promising mechanical strength. However, these strategies raise the concerns of cost and processing complexity. Developing cost-efficient methods for large-scale fabrication of superhydrophobic surfaces with favorable mechanical stability and easy reparability is highly desirable. Recently, we have proposed a thermal spray route for constructing novel superhydrophobic coatings [17,18], providing the possibilities of fabricating large-scale superhydrophobic surfaces using a wide variety of engineering materials deposited on various substrates [19,20].

The idea of constructing superhydrophobic surfaces with mechanically robust and easy-repairable performances is inspired from natural hydrophobic surfaces which are able to self-heal both their structures and surface chemistry after damaged. Several recent studies report the surfaces with a roughness at two length scales to ensure that hydrophobicity retains well even after some surface features are worn away [21–23]. In this study, we present a new superhydrophobic surface with multiple length-scale structure for enhanced mechanical strength and ease of healing after destruction. Titania coating with the surfaces in cone geometry was made by plasma spray, followed by suspension flame spray deposition of polytetrafluoroethylene (PTFE)/copper nanoparticles (nano-Cu) as a top layer. The hydrophobicity and mechanical strength of the surfaces were systematically assessed and elucidated.

## 2. Experimental

Commercial titania powder with the size range of +15–45  $\mu\text{m}$  (Sun-spraying Science and Technology Co., Ltd., China) was used as the starting feedstock for coating fabrication. The coatings were deposited by atmospheric plasma spray (APS–2000 K, Beijing Aeronautical Manufacturing Institute, China) on stainless steel plates (316L). The plasma net energy of 30 kW was used for fabricating the coatings. Micropatterned topographical features of the coatings were achieved using stainless steel mesh as shielding plate. The meshes with the size of 74  $\mu\text{m}$ , 125  $\mu\text{m}$ , and 173  $\mu\text{m}$  were used in turn for constructing cone-like geometry. Argon was used as the primary gas and the powder carrier gas with the flow rate of 42 l/min and 4 l/min, respectively. The auxiliary gas was hydrogen with the flow rate of 11 l/min. The powder feeding rate was 50 g/min and the spray distance was 150 mm. Further fabrication of a PTFE/nano-Cu layer was made on the pre-micropatterned titania coatings. PTFE/nano-Cu suspension was employed for the coating deposition according to an established protocol by suspension flame spray [17]. The FS-4 flame torch (Wuhan Research Institute of Materials Protection, China) was employed for the spraying. For preparing the PTFE/nanoparticles suspension, Cu nanoparticles with the size of  $\sim 835$  nm in mean diameter (Xinshengfeng Technology Co., China) were added into alcohol. The suspension with Cu concentration of 5.0 wt.% and PTFE (Zhejiang Juhua Co., China) concentration of 5.0 wt.% were prepared.

Microstructure of the coatings was characterized by field emission scanning electron microscopy (FESEM, FEI Quanta FEG250, the Netherlands). Chemical composition of the samples was detected

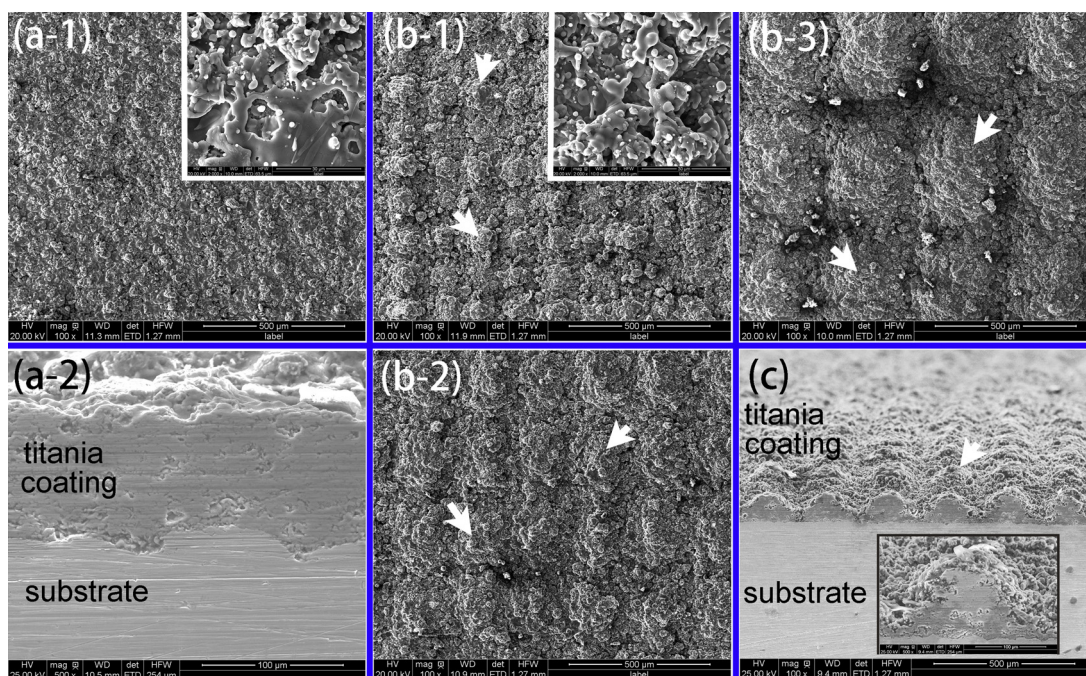
by X-ray diffraction (XRD, Bruker AXS, Germany) using Cu K $\alpha$  radiation operated at 40 kV and 40 mA. Contact angle and sliding angle measurements were carried out using a video-based optical system (Dataphysics OCA20, Germany). The numerical values were measured at room temperature after water droplet was knocked down onto the surface of the samples. Volume of each distilled water droplet was 5  $\mu\text{l}$  for contact angle measurement and 15  $\mu\text{l}$  for sliding angle measurement. For every contact/sliding angle for each sample, five measurements were made from different surface locations. Sizes of the starting particles were examined using Zetasizer Nano ZS (Malvern Instruments, UK). Mechanical durability of the constructed coatings was assessed by scratch testing method, which has been extensively used for evaluating hydrophobic surfaces [24–29]. 800 # sandpaper was used as the abrasion surface. The hydrophobic surfaces were tested facing the sandpaper with varying sliding distances under an applied pressure of 25 kPa.

## 3. Results and discussion

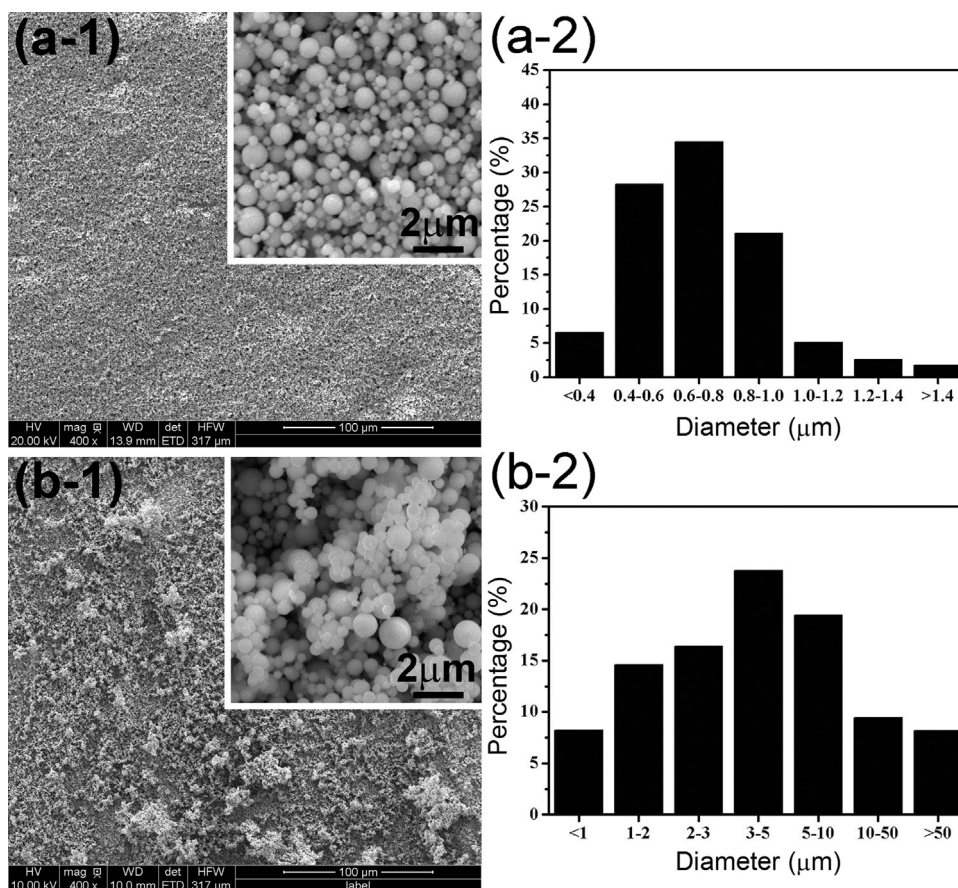
To comparatively investigate the influence of topography of the surfaces on their hydrophobicity and mechanical durability, the as-sprayed titania coatings without the assistance of stainless steel mesh were also fabricated. The as-sprayed titania coatings display relatively smooth topographical morphology with typical rough microstructure (Fig. 1a-1) and their thickness is tunable by easily controlling the spray processing (e.g.,  $\sim 90$   $\mu\text{m}$  as shown in Fig. 1a-2). Two length-scaled topographical morphology of the titania coatings was successfully fabricated with the aid of the mesh shielding during the plasma spraying (Fig. 1b and c). The unique micropatterned surfaces show clearly the cone-like structural features with two length scales profile. The mesh size decides crucially the key topographical features of micropatterned titania coatings, namely the height and root diameter of the cones and the distance between two adjacent cones. The unique protrusions exhibit the diameter of  $\sim 128$   $\mu\text{m}$  (Fig. 1b-1),  $\sim 192$   $\mu\text{m}$  (Fig. 1b-2),  $\sim 342$   $\mu\text{m}$  (Fig. 1b-3) at root and are sharp at top, respectively, depending on the size of the shielding mesh used for the fabrication of the surfaces. Cross-sectional view of the cone geometry shows clearly unique structural feature (Fig. 1c and the enlarged view shown as the inset in Fig. 1c). In addition, almost identical microstructures are seen for all the coatings (insets in Fig. 1a-1 and b-1), which suggest porous nature of the microenvironment on the surfaces of the constructed coating matrix. The micro-porous structures provide ideal platform for settlement of additional nanomaterials. These features should affect performances of the coatings.

Further modification of the as-sprayed titania coatings was done by the suspension flame spray deposition of PTFE/nano-Cu composites. Morphologies and size distribution of the untreated and PTFE treated Cu nanoparticles are shown in Fig. 2. The starting well-dispersed Cu nanoparticles have the size of  $\sim 835$  nm in mean diameter (Fig. 2a). After the PTFE treatment, Cu particles get notably aggregated, showing the size of  $\sim 15.3$   $\mu\text{m}$  in mean diameter (Fig. 2b). XRD characterization of the untreated titania coatings suggests presence of anatase and rutile (Fig. 3a), indicating certain transformation of anatase to rutile during the plasma spraying. This is normal since anatase transforms to rutile at elevated temperatures. Indeed the phases do not matter in this case. The additional construction of the PTFE/nano-Cu layer is further evidenced by the XRD detection (Fig. 3b). The results show successful modification of the titania coatings with the PTFE/nano-Cu top layer.

Wettability assessment revealed superhydrophilic nature of the as-plasma sprayed titania coatings with a water contact angle of less than  $10^\circ$ , regardless of additive patterning or not. After the further construction of the PTFE/nano-Cu top layer, all the coatings display superhydrophobicity with water contact angle (CA) of

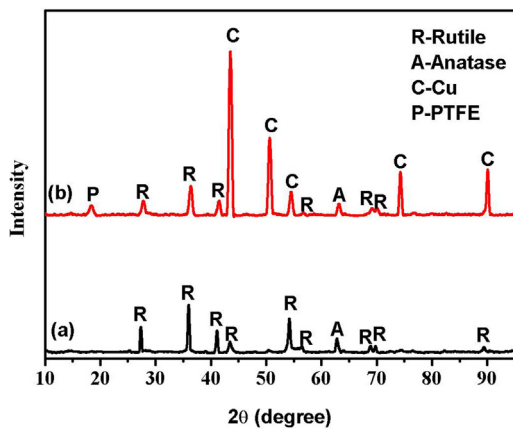


**Fig 1.** FESEM images of the coatings showing (a-1) surface morphology and (a-2) cross-sectional morphology of the titania coating, (b-1, b-2, b-3) surface morphology of the titania coatings fabricated with the mesh shielding, and (c) cross-sectional morphology of the coating (b-2). The size of the steel meshes used is 74  $\mu\text{m}$ , 125  $\mu\text{m}$ , and 173  $\mu\text{m}$  for the coating (b-1), (b-2), and (b-3), respectively. The insets in (a-1), (b-1), and (c) are enlarged views of selected areas of the images respectively. The white arrows point to typical cones.



**Fig. 2.** SEM images and size distribution of the Cu particles before (a) and after (b) the PTFE treatment. The insets are enlarged views of selected areas correspondingly.





**Fig. 3.** XRD curves of (a) the as-sprayed titania coating and (b) the PTFE/nano-Cu modified titania coating.

**Table 1**

Contact angle and sliding angle of water droplets tested on the coatings.

Samples	Contact angle/°	Slide angle/°
Coating A	<10	–
PTFE/nano-Cu layer alone	152.5	4
PTFE/nano-Cu on coating A	152.8	3.5
PTFE/nano-Cu on coating B	152.7	2
PTFE/nano-Cu on coating C	152.6	2
PTFE/nano-Cu on coating D	153.3	2

Coating A: the titania coating with normal surface structure; coating B: the titania coating with surface cone geometry made with 74  $\mu\text{m}$  mesh shielding; coating C: the titania coating with surface cone geometry made with 125  $\mu\text{m}$  mesh shielding; coating D: the titania coating with surface cone geometry made with 173  $\mu\text{m}$  mesh shielding.

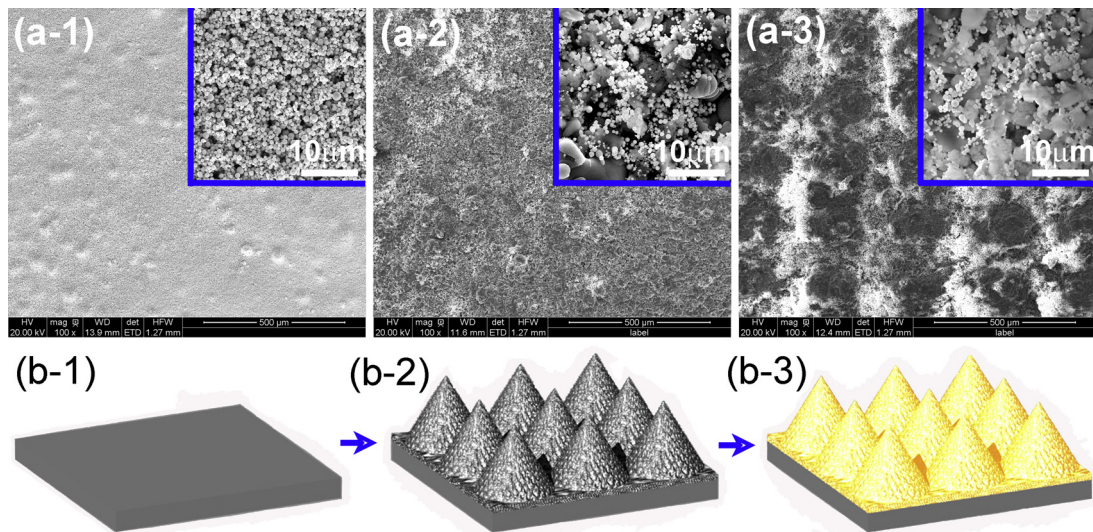
$\sim 153^\circ$  and sliding angle (SA) of lower than  $4^\circ$  (Table 1). In addition, the patterned titania coating with the PTFE/nano-Cu top layer shows a SA of  $\sim 2^\circ$ , more slippery than other surfaces without the cone geometry. Synergistic effect of the cone-like topographical matrix structure and the PTFE/nano-Cu layer is suggested for the superhydrophobicity.

To elucidate the superhydrophobic characteristics of the surfaces, microstructure examination was carried out. SEM observation clearly shows the top layer with alternative morphologies (Fig. 4a). For comparison purposes, the PTFE/nano-Cu composites were also sprayed directly on glass plate (Fig. 4a-1). It is not surprising that the PTFE/nano-Cu layer shows nanostructures similar to the starting particles (inset in Fig. 4a-1 versus Fig. 2b-1). However, micro-/nano- hybrid topographical structures are obviously fabricated after deposition of the PTFE/nano-Cu layer on the titania coatings (Fig. 4a-2 and a-3). PTFE/nano-Cu has colonized evenly on the cones and inside the caves existing in the surface layer of the coatings, and diffusion into the pores within the coatings is also seen (the insets in Fig. 4a-2 and a-3). It is clear that the pre-patterned titania coatings exhibit significantly reinforced multiple length-scale topography after the construction of PTFE/nano-Cu layer. The distinct multiple length-scale topography should account for the significantly enhanced hydrophobicity. This result is consistent with a previous study that the structures in the sizes of more scales possess more efficient self-cleaning performances [6].

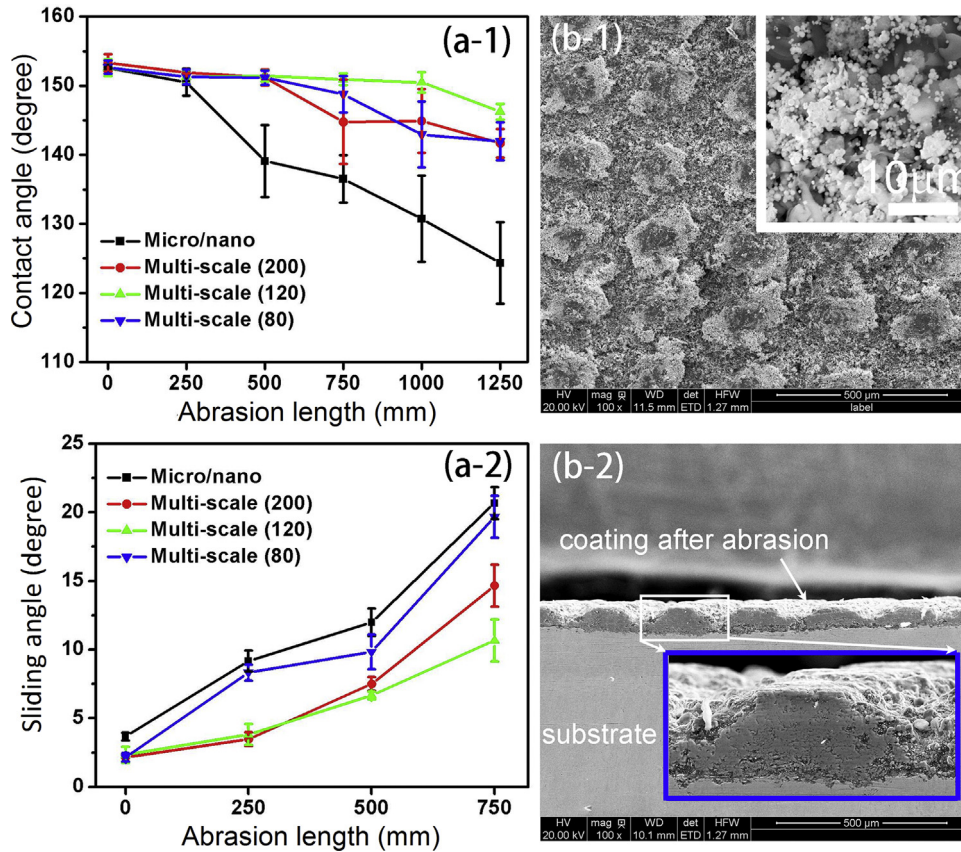
The multiple length-scale superhydrophobic structure constructed by thermal spray approach is schematically depicted (Fig. 4b). The superhydrophobic coatings can be constructed on a wide variety of substrate materials, metals, ceramics, or polymers, et al. (Fig. 4b-1). The inorganic matrix coatings with microporous topographical structures and micron-sized cone geometry are made by thermal spray approach (Fig. 4b-2). Further modi-

fication by suspension thermal sprayed PTFE/nano-Cu facilitates accomplishment of superhydrophobicity of the coatings (Fig. 4b-3). Obviously, sizes, spacing and shapes of the structures affect predominately wettability of the surfaces. The cone geometry in the size of tens of microns essentially performs the function as rough hydrophobic skeleton and supplies mechanical strength. Further decoration by PTFE/nano-Cu as the thin top layer provides nanostructures and low energy materials. It was realized that cone-like structure in nanoscale features also produces superhydrophobicity [30], even though if the superhydrophobic surfaces can hold up against surface damage is still a challenging question. It has been reported that conical surface textures exhibit a spontaneous, partial reappearance of trapped gas phase upon liquid depressurization, yet the superhydrophobic state of the nanostructured conical textures vanishes above critical pressures which depend on texture shape and size [31]. The mechanism as to how nanostructured geometry offers superhydrophobicity is believed to be attributed to partially trapped air inside the nanostructures, which in turn gives rise to incomplete liquid penetration [32]. Our technique route equips the inorganic matrix coatings with tunable surface textures in micron-sized scale and additional hydrophobic surface chemistry. The low energy PTFE layer with nanostructures inhibits possible infiltration of water droplets, facilitating a long-term hydrophobicity. It is noted, however, that the wettability of the constructed surfaces depends to a large extent on the spacing between adjacent cones (Table 1), which needs to be further elucidated. The most exciting advantage of the approach proposed in this research is the wide selection of substrate materials and inorganic coating materials, simplicity in fabrication and efficiency in cost.

Mechanical damage of superhydrophobic surfaces usually results in increased sticking of water, leading to loss of hydrophobicity. The PTFE/nano-Cu coating alone on glass plate can be easily removed by finger scratching. While mechanical durability of the superhydrophobic surfaces constructed on titania coatings was examined by scratch testing. The evolution of CA and SA of water droplets on the superhydrophobic surfaces as a function of the abrasion length is shown in Fig. 5. To quickly assess mechanical stability of the superhydrophobic surfaces, a relatively high load pressure of 25 kPa was employed for the examination. It is clear that CA of all the surfaces is constrained by the abrasion (Fig. 5a-1). With increase in abrasion length, CA of the normal titania coating covered by the PTFE/nano-Cu top layer drops markedly, showing a value of  $\sim 130^\circ$  as the abrasion length is 0.5 m. Surprisingly, all the surfaces constructed on the patterned titania coatings retain the superhydrophobicity with a water contact angle of  $\sim 150^\circ$ . SA values of all the surfaces obviously increase with the increase in abrasion length (Fig. 5a-2). Compared with CA, SA values are more sensitive to the abrasion. When the abrasion length is increased to 0.5 m, SA of the normal titania coating increases significantly from  $\sim 3.5^\circ$  to  $\sim 12^\circ$ . While SA values of all the surfaces constructed on the patterned titania coatings are lower than  $10^\circ$  as the abrasion length is 0.5 m. It is noted that the micropatterned topographical features are remained well after the abrasion (Fig. 5b-1, b-2), predominately due to the fact that as typical ceramic material, titania offers remarkable capability of resisting wear. After long time abrasion, only the sharp top end parts of the cones are worn off, majority of the cone geometry is retained. Consequently, most of the micro-/nano-scaled topographical morphologies and the surface chemistry are largely protected. The nanoscaled structure and surface chemistry of the low surface energy hydrophobic layer can be further preserved by the microporous structure and microscaled titania in between the protrusions (see the enlarged surface view shown as inset in Fig. 5b-1). It is therefore anticipated that as far as the patterned structural features are still there, the superhydrophobicity of the surfaces persists. It is therefore clear that the



**Fig. 4.** Topographical morphologies of the samples (a-1, a-2, a-3) and schematic illustration showing thermal spray construction of the superhydrophobic coatings (b). (a-1) PTFE/nano-Cu layer was directly deposited on glass plate (the inset is enlarged view of selected area), (a-2) PTFE/nano-Cu layer was deposited on the normal titania coating, and (a-3) PTFE/nano-Cu layer was deposited on the patterned titania coating (the inset is enlarged view of selected area). (b-1, b-2, b-3) depicts the wide selection of substrate materials, simple deposition of the coatings with cone geometry, and further modification of PTFE/nano-Cu to achieve superhydrophobicity.



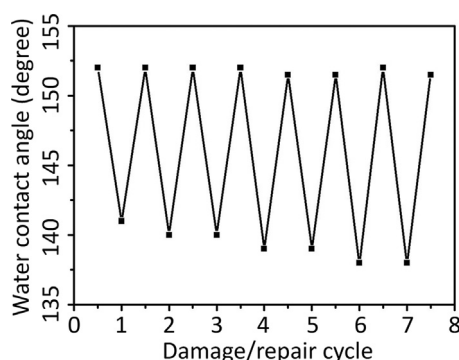
**Fig. 5.** Water contact angle (a-1) and sliding angle (a-2) of the superhydrophobic surfaces versus the abrasion length under the applied pressure of 25 kPa. (b-1, b-2) SEM images of the superhydrophobic surfaces after abrasion showing structural changes of the cone geometry after severe abrasion (the insets are enlarged views of selected areas).

durability of the superhydrophobicity of the constructed surfaces in harsh wear service environment is mainly decided by mechanical strength of the matrix coating materials (titania in this case). Furthermore, it is interesting to note that the surfaces constructed on the titania coating with the inter-distance between adjacent cones of  $\sim 227.5 \mu\text{m}$  show the best hydrophobic performances after

severe abrasion (Fig. 5a). This indicates the remarkable influence of the pattern size on wettability, which has also been realized by other researchers [33–36].

In addition to the mechanical durability, easy reparability is another essential variable for a superhydrophobic surface for long-term functional services [37–39]. In this study, the dam-





**Fig. 6.** Water contact angle of the hydrophobic surfaces with cone geometry versus the number of damage/repair cycle.

aged superhydrophobic surfaces with multi-scale structures can be easily recovered by further suspension flame spray deposition of PTFE/nano-Cu. The hydrophobicity of the coatings deteriorates after severe abrasion, showing a water contact angle of  $\sim 140^\circ$  (Fig. 6). After one more time suspension flame spray deposition of PTFE/nano-Cu, the damaged surfaces are restored and this process allows the coatings to once more display superhydrophobicity. This reparability is repeatable and works for many cycles (Fig. 6). It is clear that in the first 7 cycles of damage-repair treatment, increase in the treatment cycle triggers slight decrease in CA of the damaged surfaces. Nevertheless, the surfaces are still hydrophobic in nature. This easy-reparability characteristic is important for practical applications of the superhydrophobic surfaces in harsh environment.

#### 4. Conclusions

Patterned titania coatings with cone-like geometry have been fabricated by plasma spray. And further modification of the coatings by PTFE/nano-Cu as top layer deposited by suspension flame spray results in significantly enhanced hydrophobicity. Superhydrophobic surfaces with multi-scaled structures have been constructed and the surfaces possess both favorable mechanical stability and easy reparability. The multi-scaled surfaces exhibit the superhydrophobicity with a high CA ( $\sim 153^\circ$ ) and a low SA ( $\sim 2^\circ$ ). The results shed light on constructing large-scale wear-resistant superhydrophobic surfaces by thermal spray approach for long-term functional applications.

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